

Impressão por escrita direta utilizando binder reativo baseado na resina de Pechini para a obtenção de suportes catalíticos de SnO₂ de fase pura

Pechini-based reactive-binder ceramic suspension for direct ink writing of phase-pure structured SnO₂ catalyst supports

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Resumo

O óxido de estanho (SnO₂) é um óxido metálico quimicamente estável e ativo em processos oxirredutivos, amplamente utilizado como suporte catalítico em reações heterogêneas, detecção de gases e aplicações relacionadas à energia. Neste trabalho, apresentamos uma abordagem inovadora para a manufatura aditiva de suportes catalíticos estruturados de SnO₂ por extrusão de pasta cerâmica (DIW), utilizando um ligante reativo derivado do método de Pechini. A formulação da pasta combina pó comercial de SnO₂ com um complexo polimerizável de estanho, ácido cítrico e etilenoglicol, que atua simultaneamente como modificador reológico e precursor metálico. Essa dupla função elimina a necessidade de agentes plasticizantes inertes ou ligantes à base de óxidos não-nativos. A pasta resultante apresenta propriedades viscoelásticas adequadas para conformação por extrusão e, após calcinação, o ligante se decompõe e se converte em SnO₂, complementando a carga sólida inicial. As peças sinterizadas mantêm sua integridade geométrica, tornando-se ideais para aplicações catalíticas que exigem alta estabilidade térmica e química. Essa estratégia de ligante reativo oferece uma rota simples, escalável e quimicamente limpa para a fabricação de componentes estruturados à base de óxidos metálicos, com potencial de aplicação em sistemas monometálicos ou óxidos mistos.

palavras-chave: Óxido de estanho, Impressão 3D, Ligante reativo

Abstract

Tin oxide (SnO₂) is a chemically stable, redox-active metal oxide widely employed as a catalyst support in heterogeneous reactions, gas sensing, and energy-related applications. Here, we present a novel approach for the additive manufacturing of structured SnO₂ catalyst supports via direct ink writing (DIW), utilising a Pechini-derived reactive binder. The ink formulation combines commercial SnO₂ powder with a polymerisable complex of tin, citric acid, and ethylene glycol, which functions both as a rheological modifier and as a metal oxide precursor. This dual role eliminates the need for inert thickeners or non-native oxide binders. The resulting paste exhibits suitable viscoelastic properties for extrusion-based shaping and, upon calcination, the binder decomposes and converts to SnO₂, complementing the original solid loading. The sintered pieces retain their geometric integrity, rendering them ideal for catalytic applications requiring high thermal and chemical stability. This reactive-binder strategy offers a straightforward, scalable, and compositionally clean route to structured metal oxide components, with potential applicability to other single or mixed oxide systems.

Key-words: Tin oxide, Direct Ink Writing, reactive binder

1. INTRODUCTION

Energy Transition is possibly one of the biggest challenges that we face as a society in the 21st century. Driven by extreme climate events attributed to rising atmospheric CO₂ levels, promoted by the extensive use of oil- and coal-derived combustion, this new transition pushes us to find alternative energy systems and routes to produce materials essential for our modern society. Overcoming this challenge requires a collective and multidisciplinary effort, of which the design of robust, efficient and sustainable catalysts is a major example.

Recent works from our group have explored the synthesis and application of metal oxides in processes relevant to Energy Transition, including the conversion of CO₂ to value-added fuels ¹, and the synthesis of ammonia from dissolved N₂ in ambient conditions ², where they act as catalysts. In earlier development stages, the catalysts are typically synthesized in powder form, but for achieving higher technological readiness levels and facilitate out-scaling, having them in easily-handled forms is essential. In practical large-scale applications, solid catalysts are typically shaped into or fixed onto larger particles, such as pellets or other geometrical fillings, which are then inserted on reaction vessels. These pieces of equipment are intended to promote optimal contact between the reactants, usually fluids, and the catalysts; and the geometry of the support is designed to facilitate this process while also controlling the pressure drop through the equipment, reducing the energy demand. To fix the catalysts onto supporting materials, synthesis methods such as ultrasonic spray ³, jet-inking ⁴, spin-coating ⁵ or dip-coating ⁶ can be used. While these methods are well established, an active research area is that of tailoring the support properties and geometry.

Among the various catalyst supports reported in the literature, ceramic materials are more frequently employed due to their high thermal and chemical stability, mechanical robustness, and resistance to sintering under harsh reaction conditions. In addition, their surface chemistry can be tuned to optimize catalyst-support interactions, enhancing the dispersion, stability, and activity of the active phase. The specialized literature has shown that the nature of the support affects the performance of the catalysts, so tailoring its composition – particularly avoiding the presence of unwanted species, especially metallic ions – is a key aspect of materials processing. Studies report that supports with high surface area and tailored porosity, such as mesoporous metal oxides, promote uniform dispersion, stabilize nanoparticle size (often below 6 nanometres), and generate active metal-support interfaces that boost turnover frequencies by orders of magnitude in reactions like carbon monoxide oxidation ⁷. In addition, supports that provide oxygen vacancies, specific redox states, and controlled surface chemistry (for example, cerium dioxide and titanium dioxide) enhance oxygen activation and strengthen metal-support bonding. These features are able to improve reaction rates and also selectivity and durability in a range of industrial processes, including electrocatalysis, preferential oxidation, and steam reforming ⁸.

Several routes have been developed to produce ceramic catalyst supports with tailored composition, morphology, and surface chemistry. Advanced additive manufacturing techniques, such as extrusion-based 3D printing (*Direct Ink Writing*) and stereolithography, allow the direct fabrication of structured supports with customised geometries, optimised flow channels, and hierarchical porosity ⁹. These methods facilitate the incorporation of specific design parameters from the early stages of fabrication.

Conventional ceramic processing relies heavily on polymeric binders to impart plasticity, cohesion, and shape retention during forming. These additives, however, are transient and must be removed prior to densification, often through thermal debinding, a step that can introduce defects such as cracking, carbon retention, or anisotropic shrinkage if not carefully controlled¹⁰. Such challenges underscore the limitations of inert binders, which serve only as processing aids and contribute no functional role to the final ceramic body. In contrast, reactive binders offer a transformative alternative: they simultaneously tailor rheology during shaping and convert into the target oxide upon calcination, thus eliminating foreign species and contributing to the final solid loading¹¹. Recent developments have demonstrated their potential to yield phase-pure ceramic components while simplifying debinding and improving microstructural integrity^{12,13}. Building on this approach, we previously reported a method for preparing TiO₂ structures by direct ink writing without the use of inorganic binders, thereby avoiding the incorporation of unwanted metal cations¹², and here we extend this methodology to SnO₂, a material valued for its thermal and chemical stability, tunable electronic structure, strong metal–support interactions, and morphological flexibility. These properties make SnO₂ particularly attractive as a support for metals in electrocatalytic processes¹⁴, especially under oxidising or high-temperature conditions, NO_x reduction¹⁵, and biocatalysis¹⁶, among others.

2. METHODOLOGY

2.1 Materials

Tin(IV) oxide (SnO₂, Balestro Inc.) was used as the primary ceramic phase. Tin oxalate (SnC₂O₄, ≥98 %, Sigma–Aldrich) was employed as the inorganic precursor in the preparation of the Pechini-type polymeric resin. Citric acid (≥99.5 %, Synth), monoethylene glycol (≥99.0 %, Neon), nitric acid (65%, Synth) and deionized water were used for preparing the resin. All reagents were used without further purification.

2.2 Formulation of the ceramic paste

The extrudable SnO₂ ceramic paste was prepared by mixing a polymeric resin at 1500 rpm with dried SnO₂ powder, which was gradually incorporated to achieve the desired solid loading, followed by mixing at 2500 rpm for 60 s to ensure homogeneity. The compositions were adjusted to obtain different ratios of solids loading, 76.02%, 74.37%, 75.00% and 72.50% (SnO₂-1, SnO₂-2, SnO₂-3, and SnO₂-4, respectively).

The polymeric resin, containing a precursor for *in-situ* formation of SnO₂ nanoparticles, was prepared via a modified Pechini process¹⁷. Briefly, monoethylene glycol was heated to approximately 70 °C together with citric acid, using a magnetic stirrer. Once a homogeneous mixture was obtained, i.e., a clear, transparent solution, the sample was kept for 30 minutes in the polymerization process at 120 °C. Meanwhile, the tin oxalate solution was stirred with 23 wt% diluted nitric acid for about 1 hour in order to convert the oxidation state to +4, needed to form SnO₂ during de calcination process. Finally, the tin oxalate was slowly added to the monoethylene glycol and citric acid mixture at 120 °C, while being stirred at a constant speed with the aid of a magnetic stirrer for 30 minutes. The SnO₂ content (7.75%) of the resin was determined by calcining a resin sample at 900 °C for 5 h in air, and its water content was calculated by thermogravimetry (37.8 ± 2.2%) upon drying paste samples at 120 °C for 48 hours.

2.3 Direct ink writing

The pastes were printed using a cartesian-type 3D printer (DuraPrinter C02, Duracer) equipped with a piston-driven reservoir feeding an Auger extrusion system. Printing was carried out at a reservoir pressure of 3 bar through a 1.2 mm nozzle. The slicing was performed in Ultimaker Cura with the following parameters: layer height = 0.8 mm; initial layer height = 0.5 mm; line width = 1.2 mm; flow = 200 %; printing speed = 15 mm s⁻¹; travel speed = 30 mm s⁻¹; spiralized outer contour mode = on. No top/bottom layers were printed to obtain hollow-walled geometries. The printed test geometry was a 40 x 40 mm hollow cylinder, designed to evaluate the shape fidelity and self-support capability of the paste. After printing, samples were dried at ambient conditions for 48 h and calcined in air at 500 °C (2 °C min⁻¹) for 5 h.

2.4 Analyses

The X-ray diffraction patterns (XRD) were obtained using an X'Pert-MPD (Philips) diffractometer with Cu K α radiation, operated at 45 kV and 40 mA. The step size was set at 0.02° 2 θ per second over the 10-90° 2 θ range. The crystallite sizes and the lattice parameters were calculated by the Rietveld analysis using the X'Pert Highscore software with MgAl₂O₄ as the standard. The powder density was measured using a Micromeritics AccuPyc II 1340 He gas pycnometer after 200 purges for degassing. The specific surface area was determined by nitrogen gas adsorption at 77 K (Micromeritics Gemini III 2375), according to the Brunauer-Emmett-Teller (BET) method. The samples were degassed at 250 °C for ~12 h before the experiment using a VacPrep 061 (Micromeritics). Diffuse reflectance infrared Fourier transform (DRIFT) spectroscopy was performed using a Nicolet iS50 spectrometer to identify the functional groups adsorbed on powder. DRIFT spectra were recorded in the range of 400-4000 cm⁻¹. The rheological behaviour was measured using a HAAKE MARS 60 rheometer (Thermo Fisher Scientific) with 35 mm parallel plates and a 1 mm gap at 23 °C, following a pre-shear at 5 s⁻¹ for 30 s and a shear rate sweep from 1 to 30 s⁻¹ and back to 1 s⁻¹ to obtain flow curves and hysteresis loops.

3. RESULTS AND DISCUSSION

3.1 Preparation of the tin oxide resin

The resin was prepared as reported in section 2.2. The resulting material was a viscous, translucent yellowish liquid. Upon calcination, a white powder was obtained, with a yield of 7.75% (g SnO₂ / 100 g of resin). This powder was investigated by X-ray diffraction (XRD), as shown in **Figure 1**. Broad diffraction peaks are observed, which are characteristic of nanosized crystallites. Cassiterite (JCPDS card no. 41-1445) was the only phase identified.

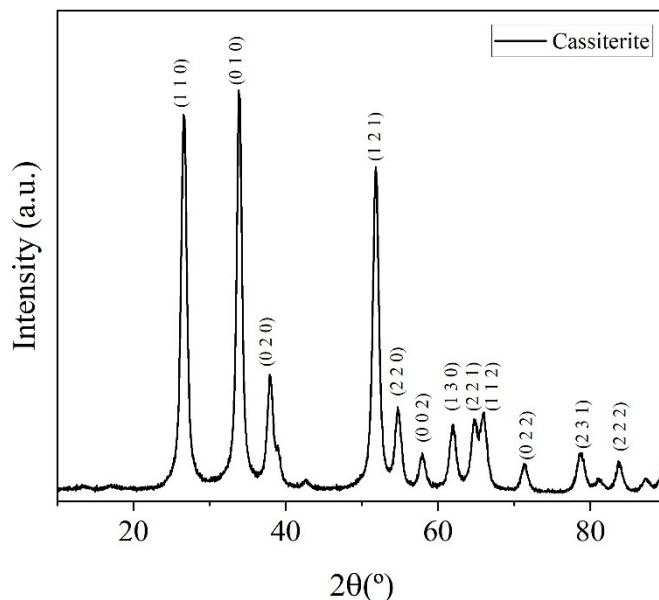


Figure 1. XRD pattern of SnO₂ nanopowders obtained upon calcination of the resin.

The average crystallite size and lattice parameters of the nanopowders were calculated after Rietveld refinement of XRD data. The estimated crystallite size was 10.71 nm, while the refined lattice parameters were $a = b = 4.7355 \text{ \AA}$ and $c = 3.1835 \text{ \AA}$. These values are in good agreement with previously reported data in the literature^{18,19}. The samples exhibited a surface area of $47.2 \pm 0.1 \text{ m}^2/\text{g}$, consistent with literature values for SnO₂ nanopowders [ref], and a density of $6.02 \pm 0.03 \text{ g/cm}^3$, lower than that of bulk SnO₂ ($6.91\text{--}6.95 \text{ g/cm}^3$) [ref], due to the nanoscale dimensions and porosity of the powders. DRIFTS spectrum of the prepared SnO₂ is given in **Figure 2**.

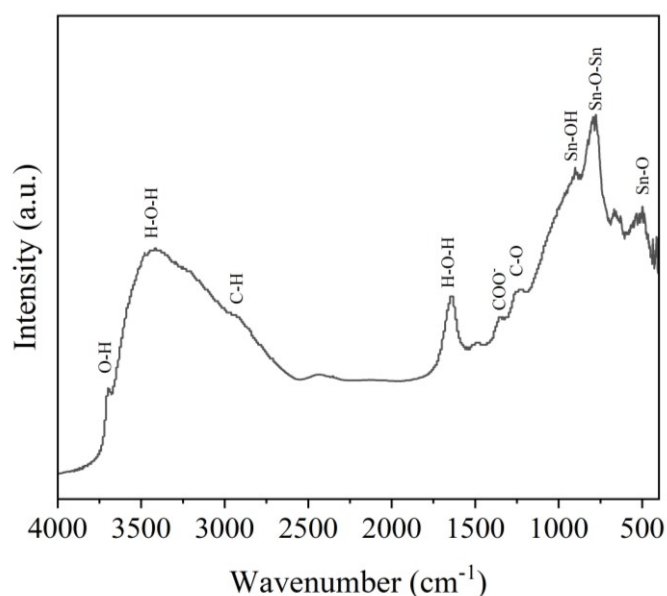


Figure 2. DRIFTS spectrum of SnO₂ nanopowder.

The IR diffuse reflectance spectrum shows a broad band at $\sim 3400 \text{ cm}^{-1}$ assigned to O–H stretching vibrations of surface hydroxyl groups and adsorbed water, while the band at $\sim 1630 \text{ cm}^{-1}$ corresponds to H–O–H bending. Weak absorptions around 2920 cm^{-1} are attributed to C–H stretching, indicating residual organic species from the synthesis. The band at $\sim 1360 \text{ cm}^{-1}$ is associated with COO[−] stretching, and a signal in $\sim 1240 \text{ cm}^{-1}$ region

corresponds to C–O vibrations, suggesting adsorbed carbonate. In the low wavenumber region, characteristic bands of Sn–O and Sn–O–Sn vibrations are observed at ~ 520 and ~ 780 cm^{-1} , confirming the formation of the Sn–O lattice.

3.2 Paste rheology

The rheological properties of the SnO₂-loaded pastes were evaluated to assess their suitability for 3D printing by direct ink writing (DIW), using SH94.4, a material with exemplary extrudable properties, as a benchmark. As shown in the flow curves in **Figure 3A**, all formulated pastes exhibited the essential pseudoplastic (shear-thinning) behaviour required for extrusion, where viscosity decreases under shear increase, enabling flow through a nozzle. This phenomenon is attributed to the alignment of polymer binder chains and the breakdown of particle agglomerates under stress^{12,20}.

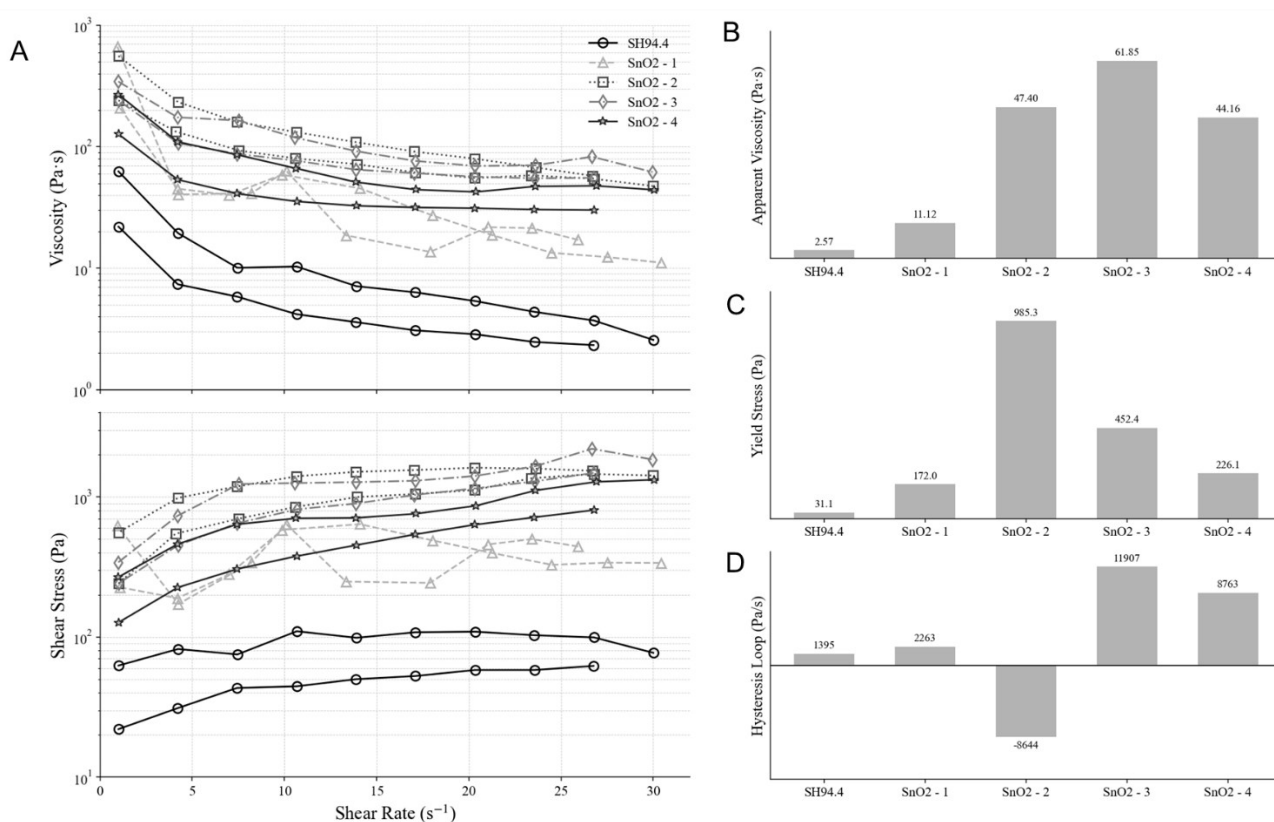


Figure 3. Rheological properties of the formulated ceramic pastes. (A) Full hysteresis loops for Viscosity and Shear Stress plotted against Shear Rate, confirming the pseudoplastic (shear-thinning) nature of all samples. The derived quantitative parameters are summarized for (B) Apparent Viscosity, (C) Yield Stress, and (D) Hysteresis Loop area. The data highlights the unique anti-thixotropic behaviour and high yield stress of the SnO₂-2 formulation.

A detailed analysis of the rheological parameters, summarized in **Figure 3B-D**, reveals critical performance differences. While the SH94.4 benchmark possesses a modest yield stress (31.1 Pa, **Figure 3C**), all SnO₂-loaded pastes offered a substantial increase. This is crucial for ensuring the shape fidelity of printed structures, as a sufficiently high yield stress allows filaments to support their own weight and the weight of subsequent layers²¹. However, an optimal rheological window exists, as an excessively high yield stress can prevent proper filament flow, leading to detrimental inter-filament porosity in the final part¹³. The most significant differentiator for DIW performance, however, is the time-dependent viscosity recovery (or *self-healing*

capacity), quantified by the hysteresis loop area (**Figure 3D**)²². The 75% solid loading paste (SnO₂-3) displayed strong thixotropic behaviour (11,907 Pa/s), far exceeding that of SH94.4. This indicates a much faster structural recovery post-extrusion, ideal for preventing filament collapse during layer-by-layer construction.

In stark contrast, the 74.37% paste (SnO₂-2) exhibited pronounced negative thixotropic behaviour, evident from its large negative hysteresis value in Figure 3d. This property indicates slower structural recovery of the paste, which can affect the shape retention of the extruded filament and ability of self-support^{20,23,24}. These findings resonate with recent meta-analyses of DIW ink design, which define a narrow “*rheological window*” where extrudability and shape fidelity coexist¹³. Barbosa et al. (2025)¹² further demonstrated that Pechini-derived polymeric binders can act dually as organic and inorganic binders, improving rheological control while contributing to oxide formation upon calcination. The present SnO₂ pastes extend this concept, evidencing those reactive binders improve viscoelastic properties and also yield a phase-pure oxide without extraneous cations, an advantage over conventional inert polymer additives.

3.3 Extrusion evaluation

Following the rheological characterization, the practical printability of each paste was evaluated using a direct ink writing (DIW) system with a 410 µm nozzle and a maximum dispensing pressure of 3 bar. The test body was a thin-walled regular cylinder, as shown in **Figure 4A**. The extrusion trials were performed to validate the rheological predictions and identify a formulation capable of forming stable, self-supporting structures.

The initial screening revealed a critical processing challenge. The pastes with higher solid loadings, 76.02% (SnO₂-1), 75.00% (SnO₂-3), and 74.37% (SnO₂-2), could not be extruded as they required a pressure exceeding the 3 bar limit, a result consistent with their high yield stresses (**Figure 3C**). Conversely, the paste with the lowest solid loading of 72.50% (SnO₂-4) was easily extrudable. However, due to its insufficient yield stress (226.1 Pa), the printed lines were not self-standing and exhibited immediate slumping, resulting in a collapsed structure as shown in **Figure 4C**. This confirmed that none of the initial formulations resided within the required rheological window for successful DIW. This behaviour parallels reports on alumina and titania DIW systems, where insufficient yield stress compromises mechanical stability of green bodies²¹.

Given that the SnO₂-3 formulation possessed the highest yield stress and therefore the greatest potential for shape retention, a slight modification was made to this paste to reduce its flow resistance just enough to enable extrusion, resulting in SnO₂-2. This optimized paste was successfully printed at approximately 2.9 bar, demonstrating both smooth deposition and excellent self-supporting properties. A thin cylindrical body structure was successfully fabricated using this formulation, as shown in the as-printed “green body” in **Figure 4D**.

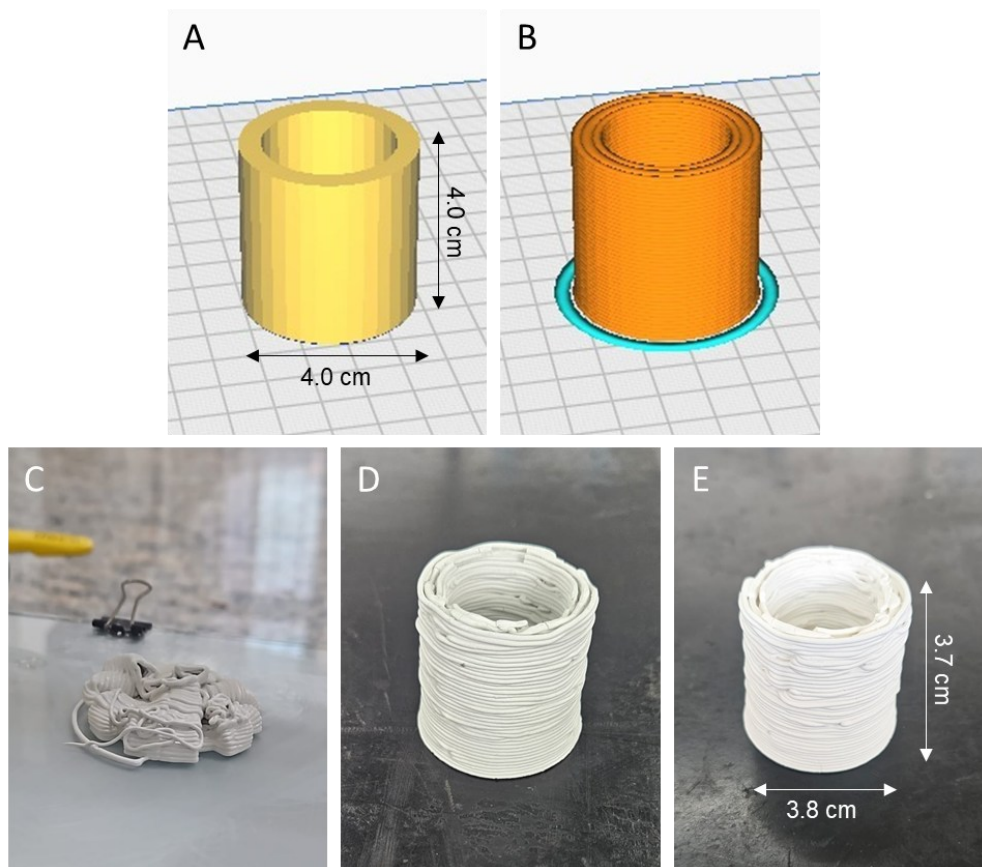


Figure 4. Direct ink writing (DIW) of SnO_2 structures showing: (a) the digital CAD model of the target geometry; (b) the sliced digital model, illustrating the G-code toolpath; (c) structural collapse of the extruded SnO_2 -4 paste; (d) the self-supporting as-printed green body fabricated using the optimal SnO_2 -2 paste; and (e) the final SnO_2 ceramic cylinder after calcination.

Finally, to obtain the dense ceramic component, the successfully printed green body was subjected to a calcination process. This thermal treatment removed the organic binder and sintered the SnO_2 particles, resulting in the final, robust ceramic structure shown in **Figure 4E**. This demonstrates the successful translation of a rheologically optimized paste into a well-defined, three-dimensional ceramic object.

The successful printing of phase-pure SnO_2 pieces represents a significant advance compared with traditional approaches, where foreign binders often introduce impurities or uncontrolled porosity. Compared to Qi et al. (2023)²⁵, who used DLP printing of Sb-doped SnO_2 electrodes to improve conductivity, the present work prioritises phase purity and structural integrity, aspects critical for catalytic applications where support composition must be tightly controlled. Moreover, unlike starch-assisted or porogen-based strategies for hierarchical porosity²², the present approach establishes a clean baseline for subsequent incorporation of pore formers or mixed oxide chemistries.

4. CONCLUSION

In this work, we demonstrated a novel strategy for the additive manufacturing of phase-pure SnO_2 supports using direct ink writing (DIW) with a Pechini-derived reactive binder. The dual role of the binder, as both a rheological modifier and an *in-situ* oxide precursor, enabled the formulation of pastes with tailored viscoelastic properties while eliminating the presence of extraneous cations typically introduced by inert binders.

Rheological analyses identified the critical balance between yield stress and thixotropic recovery required for printability, with optimized formulations enabling extrusion within operational limits and maintaining structural fidelity during layer-by-layer deposition.

The successful fabrication of self-supporting SnO₂ pieces after calcination underscores the potential of reactive-binder formulations, inspired by the knowledge of nanotechnology fields, to bridge the gap between laboratory-scale catalyst powders and structured supports. Compared with conventional shaping routes, this approach provides superior chemical purity, geometric precision, and scalability. These characteristics are particularly relevant for catalytic applications, where support composition, porosity, and integrity strongly influence dispersion, stability, and activity of the active phase.

It is expected that this study, beyond proposing a reliable strategy for preparing pure-phase 3D ceramic pieces, establishes a foundation for future work exploring hierarchical porosity, mixed oxide systems, and integration into intensified catalytic reactor designs. As such, the methodology contributes both to the advancement of ceramic additive manufacturing and to the broader effort of engineering sustainable catalyst supports for applications in energy transition technologies.

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